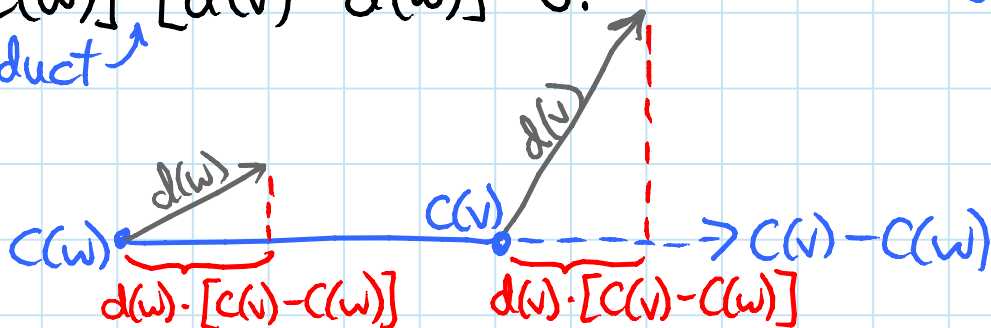


Infinitesimal rigidity: rigidity to the first order

Infinitesimal motion of a linkage configuration  $C$   
 = valid first derivative of a motion w.r.t. time, at time  $\emptyset$   
 = velocity vector  $d(v)$  for each vertex  $v$   
 preserving edge lengths to the first order:

$$[C(v) - C(w)] \cdot [d(v) - d(w)] = 0.$$

$a \cdot b \rightarrow$  dot product  $\uparrow$   
 $= a_x \cdot b_x + a_y \cdot b_y$



Rigidity matrix: "everything is linear, to the first order"  
 edge-length constraints form a linear system:

row per edge  $\left\{ \begin{array}{ccccccc} 0 & 0 & C_x(v) - C_x(w) & C_y(v) - C_y(w) & 0 & 0 & C_x(w) - C_x(v) & C_y(w) - C_y(v) & 0 & 0 \end{array} \right\} \cdot \begin{pmatrix} d_x(v_1) \\ d_y(v_1) \\ \vdots \\ d_x(v_n) \\ d_y(v_n) \end{pmatrix} = \emptyset$

$d$   $n$  columns ( $d$  dim.,  $n$  vertices)

**RIGIDITY MATRIX  $R$**

Infinitesimal motions =  $d$  for which  $R \cdot d = \emptyset$   
 = kernel  $R$  = nullspace  $R$

$\leftrightarrow$  linear subspace of some dimension: nullity  $R$

Infinitesimally rigid if nullity  $R = \binom{d+1}{2} - \binom{d-k}{2}$  where  
 config. lies in  $k$ -dim. subspace  $\mathbb{R}^d$  rigid motions / symmetries  
 (correction by student Tony Zhang in Spring 2017)

Rank-Nullity Theorem:  $\text{rank } R + \text{nullity } R = \# \text{ cols.} = d \cdot n$   
 $\Rightarrow$  inf. rigid  $\Leftrightarrow$  rank  $R = d \cdot n - \binom{d+1}{2} + \binom{d-k}{2}$  "full rank"  
 $\Rightarrow$  can test inf. rigidity in polynomial time using e.g. Gaussian elimination

Generic point set (more explicit definition than L9)  
 = all minors of rigidity matrix of complete graph induced square submatrix on subset of rows & cols. with nonzero determinant for some point set (i.e. not identically zero, algebraically) are nonzero for this point set

Generic results:

- almost every configuration is generic
- at generic configurations, rigidity = infinitesimal rigidity = generic rigidity [L9]
- $\Rightarrow$  randomized polynomial-time generic rigidity test: test infinitesimal rigidity of random realization
- if any realization is infinitesimally rigid then graph is generically rigid (else generically flexible with probability 1)

Taking derivatives: flexible  $\Rightarrow$  infinitesimally flexible  
 i.e. infinitesimally rigid  $\Rightarrow$  rigid

- but not vice versa:



Tensegrity = tens(ional int)egrity [Snelson 1968;  
R. Buckminster Fuller]

PROJECT: build tensegrity sculpture

= linkage but where each edge is either:

- bar (as before): fixed length

- cable: length can only decrease

- strut: length can only increase

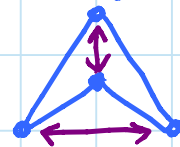
(string/  
elastic/  
spider web)

- configuration space becomes semi-algebraic

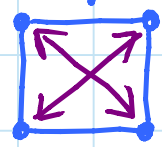
- motion, rigidity as before

- but not generic rigidity:

polynomial inequalities



vs.



flexible

rigid

- infinitesimal motion (& rigidity):

$[C(v) - C(w)] \cdot [d(v) - d(w)] = \emptyset$  for bars  $vw$

$\leq \emptyset$  for cables  $vw$

$\geq \emptyset$  for struts  $vw$

$\Rightarrow$  inf. motion space is a polyhedral cone

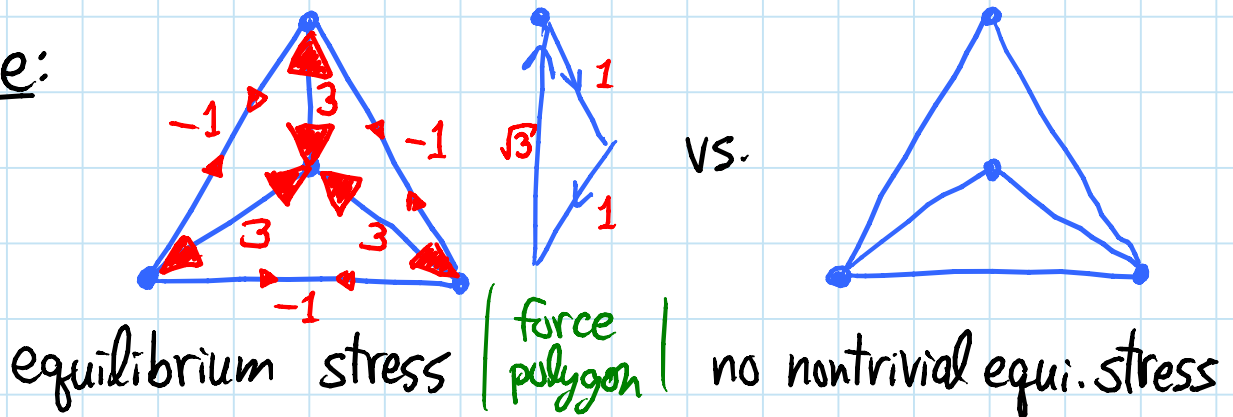
$\Rightarrow$  inf. rigidity testable in polynomial time  
via linear programming

Equilibrium stress = real number for each edge  $s: E \rightarrow \mathbb{R}$   
 such that  $s(e) \geq 0$  for cables  $e$  (push back)  
 $s(e) \leq 0$  for struts  $e$  (in resistance)

EQUILIBRIUM  $\rightarrow \sum_{w: \text{edge } vw} s(vw) \cdot [C(v) - C(w)] = 0$   
 for all vertices  $v$ .

- view  $s(vw)$  as a scale factor on force along edge  $vw$  felt equally by  $v$  &  $w$ .
  - $s(vw) > 0 \Rightarrow$  push on  $v$  &  $w$  (resist compression)
  - $s(vw) < 0 \Rightarrow$  pull on  $v$  &  $w$  (resist expansion)
  - $s(vw) = 0 \Rightarrow$  no force
- trivial equilibrium stress:  $s(e) = 0$  for all  $e$

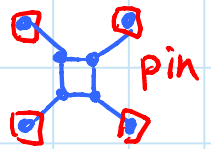
Example:



Duality in tensegrities: [Roth & Whiteley 1981]

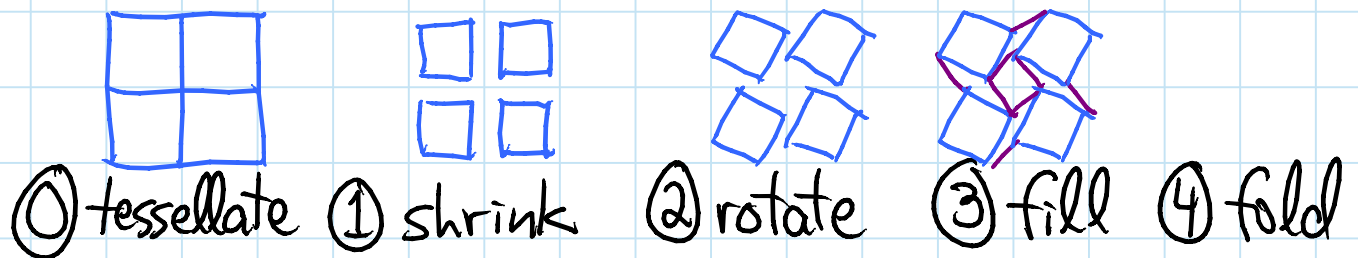
- some equilibrium stress is nonzero on strut/cable  $e$   
 $\Leftrightarrow$  every infinitesimal motion holds  $e$ 's length fixed
- tensegrity is infinitesimally rigid  
 $\Leftrightarrow$  every strut/cable is nonzero in some equilibrium stress  
 & corresponding linkage is rigid
- $\hookrightarrow$  replace cables & struts with bars } not necessary for "spiderweb" (next page)
- proofs based on linear-programming duality

Spiderwebs: all-positive equilibrium stress  
(except on boundary)  
⇒ infinitesimally rigid [Connelly 1982]



Origami tessellations:

- much history [Momotani 1984; Fujimoto 1982; Huffman 1960s, 1978; Resch 1968; Barreto 1997; Palmer 1997; Bateman 1990s; Verrill 1990s; Lang 2000s; Gjerde 2009]
- shrink-rotate algorithm:



- works for some shrink/rotate amounts  
⇔ tessellation is a spiderweb  
[Lang & Bateman 2010]

## Polyhedral lifting of a noncrossing configuration

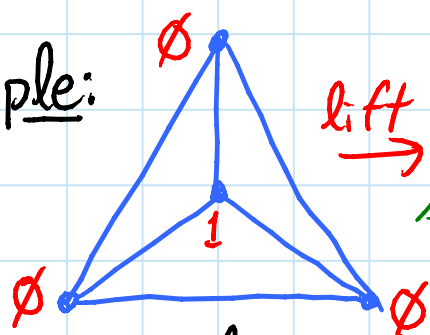
=  $z$  coordinate for each vertex  $z: V \rightarrow \mathbb{R}$

such that each face remains planar

- assume outside face at  $z=0$  by rigid motion

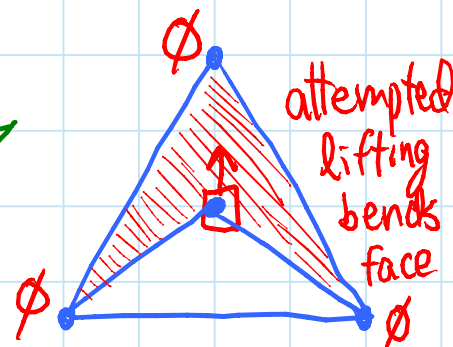
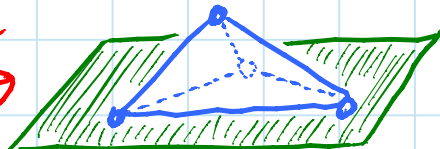
- trivial lifting:  $z(v)=0$  for all  $v$

Example:



polyhedral lifting

lift  $\rightarrow$

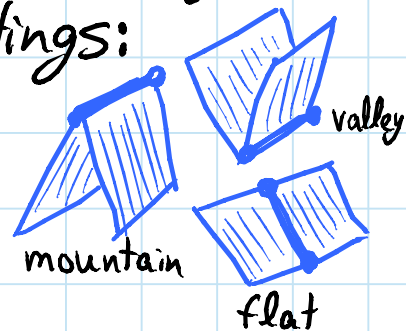


no nontrivial poly. lifting

## Maxwell-Cremona Theorem: [Maxwell 1864; Cremona 1872]

one-to-one correspondence in noncrossing tensegrity between equilibrium stresses & polyhedral liftings:

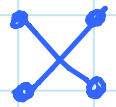
- negative stress  $\leftrightarrow$  valley edge
- positive stress  $\leftrightarrow$  mountain edge
- zero stress  $\leftrightarrow$  flat edge



**PROJECT:** implement program to illustrate stress  $\leftrightarrow$  lifting correspondence and/or stress  $\leftrightarrow$  inf. motion correspondence

**PROJECT:** virtual tensegrity building toy  
- illustrate infinitesimal flexibility if any

## Noncrossing linkages:

- configuration cannot have crossing edges 
- config. space smaller; still semi-algebraic

## Locked linkage if config. space is disconnected

i.e. no motion between some two configurations

- summary:

[L1]

2D

chains  
never locked

trees  
can lock

3D

can lock

can lock

4D<sup>+</sup>

never locked

never locked

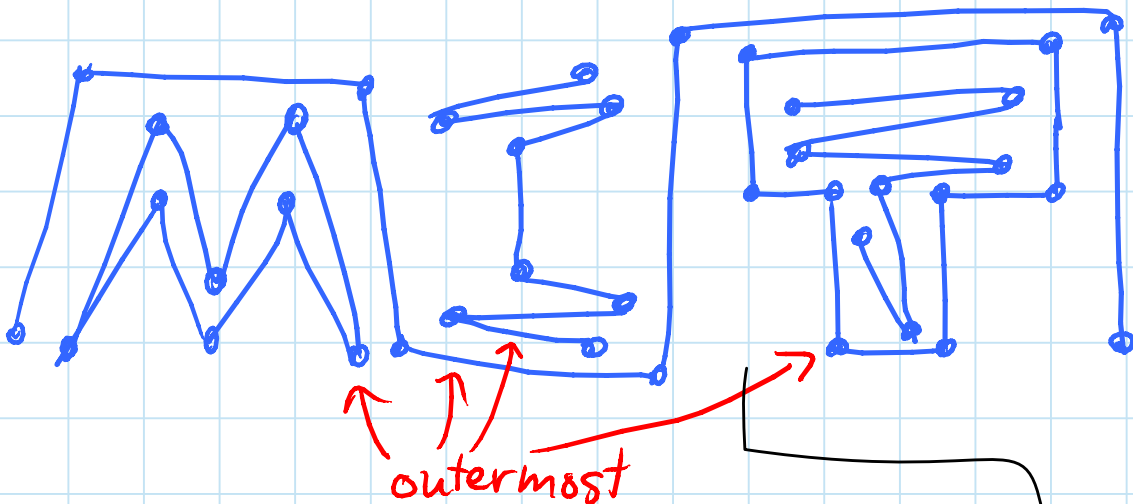
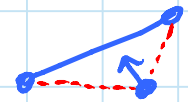
## Carpenter's Rule Theorem: [Connelly, Demaine, Rote 2000/7 2003]

any linkage configuration of maximum degree 2 has a motion that

- straightens/convexifies all outermost open/closed chains

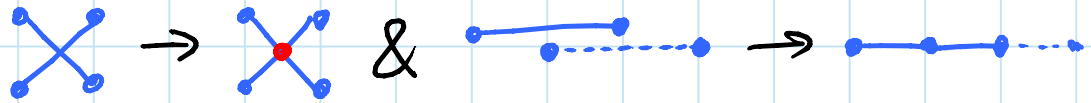
- is expansive: distance between any two vertices only increases

⇒ is noncrossing, by  $\Delta$  inequality

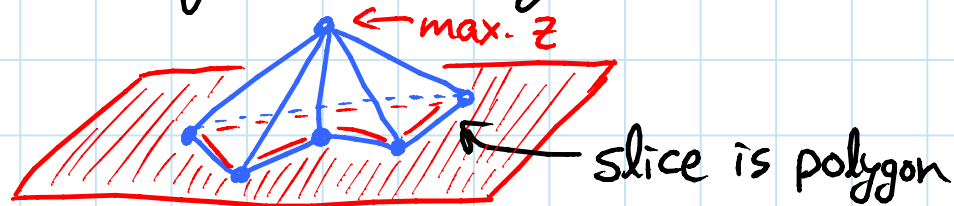


# Proof sketch of Carpenter's Rule Theorem:

- build tensegrity from linkage (edges  $\rightarrow$  bars)  
+ all possible struts (except where bar exists)
- linkage has expansive infinitesimal motion  
 $\Leftrightarrow$  tensegrity is infinitesimally flexible  
 $\Leftarrow$  every equilibrium stress is zero (on struts)  
 $\Leftrightarrow$  every polyhedral lifting is flat (on struts)
  - detail: need to show stresses are equivalent in tensegrity vs. planarized tensegrity



- here is where nested components get discarded
- slice hypothetical polyhedral lifting near max.  $z$ :
  - peak case:



- convex vertices  $\Leftrightarrow$  mountain edges
- reflex vertices  $\Leftrightarrow$  valley edges
- every polygon has  $\geq 3$  convex vertices  
 $\Rightarrow \geq 3$  incident mountains (positive stress)  
 $\Rightarrow \geq 3$  incident bars (no cables)
- but max. degree 2
- general case:   
 $\Rightarrow$  flat except inside convex polygons
- integrate ordinary differential equation  $\rightarrow$  expansive motion