## MASSACHVSETTS INSTITVTE OF TECHNOLOGY Department of Electrical Engineering and Computer Science 6.01—Introduction to EECS I Fall Semester, 2007

#### Lecture 9 Notes

# **Op-Amps**

So far, we have considered circuits with resistors and voltage sources. Now we are going introduce a new component, called an *operational amplifier* or op-amp, for short. We are studying op-amps because they are a very important circuit element, as well as because they will allow us to explore a sequence of models of how they work. These models vary in complexity and fidelity. The simplest is the easiest to use for basic circuit designs, but does not capture some important behavioral properties. The more complex models give us a more complete picture, but are often unnecessarily complicated. There is no right model of an op-amp: it all depends on the question that you are trying to answer.

#### Basic model

Figure 1(a) shows a diagram of our simplest op-amp model. The basic behavioral model is that it adjusts  $v_{out}$  in order to try to maintain the constraint that  $v_+ \approx v_-$  and that no current flows in to  $n_+$  or  $n_-$ .



Figure 1: Basic op-amp models

The best way to understand why we might want such a device is to see how it behaves in some small circuit configurations.



Figure 2: Basic op-amp models

**Non-inverting amplifier** Not surprisingly, a primary use of an op-amp is as an amplifier. Here is an amplifier configuration, shown in figure 1(b). Let's see if we can figure out the relationship between  $v_{in}$  and  $v_{out}$ . The circuit constraints tell us that

$$\nu_{-} = i_{\rm I} R_{\rm I} \tag{1}$$

$$\nu_{-} - \nu_{\text{out}} = i_{\text{F}} R_{\text{F}} \tag{2}$$

$$i_{I}+i_{F} = 0 \tag{3}$$

$$\nu_{\rm in} = \nu_- \tag{4}$$

The KCL equation 3 has no term for the current into the op-amp, because we assume it is zero. Equation 4 is the op-amp contraint. So, we find that

$$v_{\rm out} = v_{\rm in} \frac{R_F + R_I}{R_I}$$

This is cool. We've arranged for the output voltage to be greater than the input voltage, and we can arrange just about any relationship we want, by choosing values of  $R_F$  and  $R_I$ .

We can think intuitively about how it works by examining some cases. First, if  $R_F = 0$ , then we'll have  $v_{out} = v_{in}$ , so there's not a particularly interesting change in the voltages. This is still a useful device, called a *voltage follower*, which we'll study a bit later.

Now let's think about a more interesting case, but simplify matters by setting  $R_F = R_I$ . We can look at the part of the circuit running from  $V_{\rm out}$  through  $R_F$  and  $R_I$  to ground. This looks a lot like a voltage divider, with  $\nu_-$  coming out of the middle of it. Because  $\nu_-$  needs to be the same as  $\nu_{\rm in}$ , and it is  $\nu_{\rm out}$  being divided in half, then  $\nu_{\rm out}$  clearly has to be  $2\nu_{\rm in}$ .

**Inverting amplifier** Figure 2(a) shows a very similar configuration, called an *inverting amplifier*. The difference is that the + terminal of the op-amp is connected to ground, and the we're thinking of the path through the resistors as the terminal of the resulting circuit. Let's figure out the relationship between  $v_{in}$  and  $v_{out}$  for this one. The circuit constraints tell us that

$$\begin{array}{rcl} \nu_{\rm in} - \nu_{-} &=& \mathfrak{i}_{\rm I} R_{\rm I} \\ \nu_{-} - \nu_{\rm out} &=& \mathfrak{i}_{\rm F} R_{\rm F} \end{array}$$

$$i_{F} - i_{I} = 0$$
  
 $v_{+} = v_{-}$   
 $v_{+} = 0$ 

Solving, we discover that

$$u_{\mathrm{out}} = - 
u_{\mathrm{in}} rac{R_F}{R_I}$$
 .

If  $R_F = R_I$ , then this circuit simply inverts the incoming voltage. So, for example, if  $v_{in}$  is +10V with respect to ground, then  $v_{out}$  will be -10V. Again, we can see the path from  $n_{in}$  through the resistors, to  $n_{out}$ , as a voltage divider. Knowing that  $v_{-}$  has to be 0, we can see that  $v_{out}$  has to be equal to  $-v_{in}$ . If we want to scale the voltage, as well as invert it, we can do that by selecting appropriate values of  $R_F$  and  $R_I$ .

**Voltage summer** A voltage summer<sup>1</sup> circuit, as shown in figure 2(b), can be thought of as having three terminals, with the voltage at  $n_{out}$  constrained to be a scaled, inverted, sum of the voltages at  $n_1$  and  $n_2$ . You should be able to write down the equations for this circuit, which is very similar to the inverting amplifier, and derive the relationship:

$$v_{\rm out} = -\frac{R_F}{R_I}(v_1 + v_2)$$

**Voltage follower** Figure 3(a) shows a basic *voltage follower* circuit. What will it do? We can see from basic wiring constraints that:

$$u_+ = V_c$$
 $u_{out} = v_-$ 

Adding in the op-amp constraint that  $\nu_+ = \nu_-$ , then we can conclude that  $\nu_{out} = V_c$ . So, we've managed to make a circuit with the same voltage at  $n_{out}$  as at the positive terminal of the voltage source. What good is that? We'll see in the next section.

#### Voltage-controlled voltage-source model

Let's start by thinking about using a variable voltage to control a motor. If we have a 15V supply, but only want to put 7.5V across the motor terminals, what should we do? A voltage divider seems like a good strategy: we can use one with two equal resistances, to make 7.5V, and then connect it to the motor as shown in figure 3(b). But what will the voltage  $v_{motor}$  end up being? It all depends on the resistance of the motor. If the motor is offering little resistance, say 100 $\Omega$ , then the voltage  $v_{motor}$  will be very close to  $0.^2$  So, this is not an effective solution to the problem of supplying 7.5V to the motor.

In figure 4(a), we have used a voltage follower to connect the voltage divider to the motor. Based on our previous analysis of the follower, we expect the voltage at  $n_{out}$  to be 7.5V, at least before we connect it up to the motor. But our simple model of the op-amp doesn't let us understand how

<sup>&</sup>lt;sup>1</sup>As in thing that sums, not as in endless summer.

 $<sup>^{2}</sup>$ Go back and review the discussion of adding a load to a voltage divider, if this doesn't seem clear.







(a) Motor connected to a voltage follower



(b) Op-amp as a voltage-controlled voltage source



Figure 5:

connecting the motor to the output of the follower will affect the behavior of the voltage divider or what exactly will happen to the motor.

So, now, we need a somehwat more sophisticated model of the op-amp, which is shown schematically in figure 4(b). The constraint model relates the voltages at all four terminals:

$$v_{\rm out} - v_{\rm gnd} = K(v_+ - v_-)$$
 ,

where K is a very large gain, on the order of 10,000, and asserts that

$$\mathfrak{i}_+ = \mathfrak{i}_- = \mathfrak{0}$$

We can think of  $n_{out}$  and  $n_{gnd}$  as constituting a voltage source, whose voltage is defined to be  $K(\nu_+-\nu_-)$ . We can see it as *amplifying* the voltage difference  $\nu_+-\nu_-$ . It's hard to really understand how this model works without seeing it in context. So, let's go back to the voltage follower, but think about how it works using this model. Figure 5(a) shows a voltage follower, with the VCVS model of an op-amp. We can write down the equations:

$$\begin{array}{rcl} \nu_+ &=& V_c\\ \nu_{\rm out} - \nu_{\rm gnd} &=& K(\nu_+ - \nu_=)\\ \nu_{\rm gnd} &=& 0 \end{array}$$

Solving this system, we find that

$$v_{\rm out} = V_c \frac{K}{K+1}$$

So, for large K, it has very nearly the same prediction about the output voltage as our simple model.

What did we gain by moving to this more complex model? Now we have a model of what will happen when we connect a load to the output of the op-amp. There is still no current flowing into the op-amp, and therefore no influence of the current in the part of the network connected to  $n_{\rm in}$  on the current in the part of the network connected to  $n_{\rm out}$ . An op-amp in this configuration is sometimes called a *buffer*, because it provides a buffer, or disconnect, between the currents on



Figure 6: A tale of two voltage followers

either side of it. This is a big deal; it gives us a kind of modularity in our circuits that we haven't had before, by limiting the kinds of influence of one part of the circuit on the other. The ability to partially disconnect subparts of our circuits will make it easier to do complex designs.

So, now, back to the motor. If we put our new op-amp model into the motor-control circuit, as shown in figure 5(b), things are much better. We find that  $v_{out}$ , the current into the motor is 7.5V, and because of the isolation provided by the op-amp, it will remain that way, no matter what the resistance of the motor. Further, if in fact the motor has resistance of 100 $\Omega$ , then we can find that the current through the motor  $i_{motor}$  is .075A.

## Dynamic model

Figure 6 shows two voltage followers, a "good" one and a "bad" one. If we use our simplest model to predict their behavior, in both cases, we'll predict that  $v_{out} = V_c$ . If we use the more sophisticated model we developed in the previous section, we'll predict that, for the good follower  $v_{out} = V_c \frac{K}{K+1}$ . For the bad follower, things are connected a little bit differently:

$$\begin{array}{rcl} \nu_{-} &=& V_c\\ \nu_{\rm out} - \nu_{\rm gnd} &=& K(\nu_+ - \nu_=)\\ \nu_+ &=& \nu_{\rm out}\\ \nu_{\rm gnd} &=& 0 \end{array}$$

Solving this system, we find that

$$v_{\rm out} = V_c \frac{K}{K-1}$$

Those two predictions are basically the same for large K. But, in fact, the prediction about the behavior of the bad follower is **completely bogus**! To see why, we'll actually need to make a more detailed model.

Our new model is going to take the actual dynamics of the circuit into account. We can model what is going on in an op-amp by using a difference equation to describe the value of the output at a time n as a linear function of its values at previous times and of the values of  $v_+$  and  $v_-$ .

Let's start by modeling a simple linear system that is trying to approach a target value. We saw in the lecture 6 notes that a system of the form

$$y[n] = \alpha y[n-1] + c$$

in the case where  $|\alpha| < 1$  will converge to  $c/(1 - \alpha)$ . If we let c be  $\nu_+ - \nu_-$  (assuming for a minute that they are unchanging), and let  $\alpha = (K - 1)/K$ , and define

$$\nu_{\rm out}[n] = \frac{K-1}{K} \nu_{\rm out}[n-1] + (\nu_+ - \nu_-) \ , \label{eq:vout}$$

then we have a system that will, in the limit, converge to  $K(\nu_+ - \nu_-)$ .<sup>3</sup> To allow for time-varying inputs, we can generalize this to

$$\nu_{\rm out}[n] = \frac{K - 1}{K} \nu_{\rm out}[n - 1] + (\nu_{+}[n] - \nu_{-}[n]) \quad .$$
(5)

Now, we can use this model to predict the temporal behavior of the voltage followers. Let's start with the good one.

**Good follower** In this case, we have  $\nu_+[n] = V_c$ , for all n, and  $\nu_-[n] = \nu_{out}[n]$  for all n. So, equation 5 becomes

$$\begin{split} \nu_{\mathrm{out}}[n] &= \frac{K-1}{K} \nu_{\mathrm{out}}[n-1] + (V_c - \nu_{\mathrm{out}}[n]) \\ &= -\frac{1}{K} \nu_{\mathrm{out}}[n-1] + V_c \end{split}$$

This system has natural frequency -1/K, which has magnitude less than 1, so it will converge to  $\frac{K}{K+1}V_c$ , which agrees with our previous model.

Bad follower In this case, we have  $\nu_{-}[n] = V_c$ , for all n, and  $\nu_{+}[n] = \nu_{out}[n]$  for all n. So, equation 5 becomes

$$\begin{aligned} v_{\text{out}}[n] &= \frac{K-1}{K} v_{\text{out}}[n-1] + (v_{\text{out}}[n] - V_c) \\ &= \frac{2K-1}{K} v_{\text{out}}[n-1] - V_c \end{aligned}$$

This system has natural frequency (2K - 1)/K, which has magnitude greater than 1, so it will diverge! What does divergence mean in practice? Sometimes, a bad smell and then a loud pop and then smoke.

### Models

We have seen different kinds of models here. Thévenin-equivalent models have the same voltage and resistance characteristics as the circuits they model, but may have different heat-dissipation

<sup>&</sup>lt;sup>3</sup>You should be able to show this, as an exercise.

properties (consider circuit with four parallel  $10K\Omega$  resistors: it looks the same as a single  $2.5K\Omega$  resistor from the Thévenin-equivalent perspective, but the resistors are a lot less likely to melt).

In the case of the op-amps, we saw three different models, each of which was appropriate for different levels of modeling.

Sometimes, we do design using the most abstract model, and then check our designs using a more detailed one, just in case we have forgotten something. In the case of op-amps, people have used the detailed model to understand certain standard feedback configurations that are stable, and a designer is well-advised to stick to those configurations, unless they are prepared to analyze their results using a more detailed model.