

"Design Science"





Buckminster Fuller, 1963

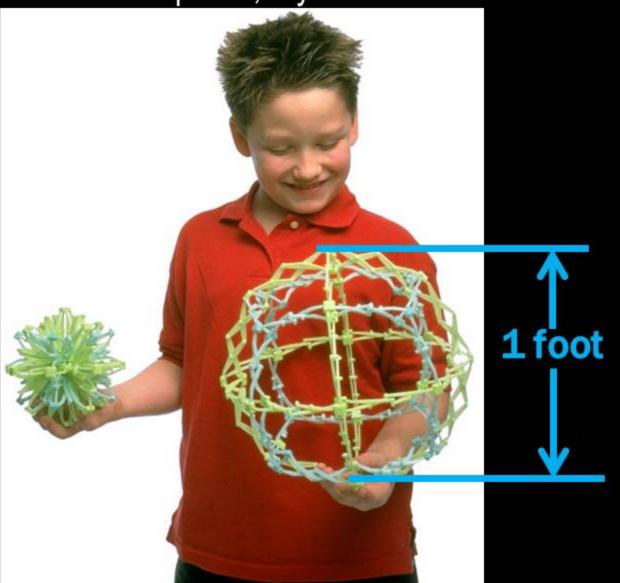


Expanding dome (Hoberman 1992)

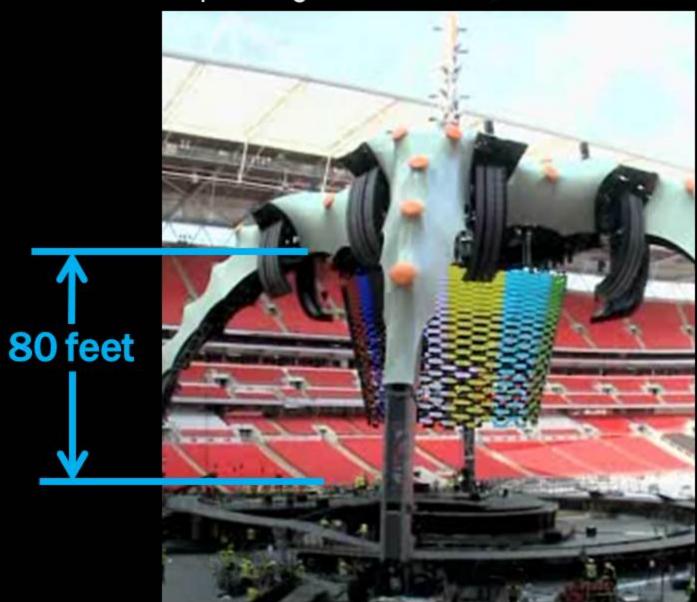
Deployable Structures



Hoberman Sphere, toy

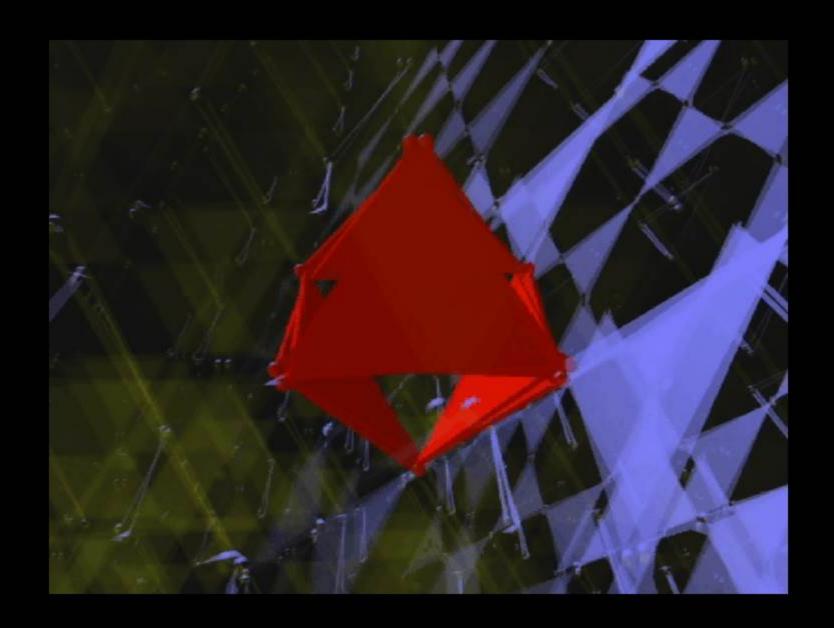


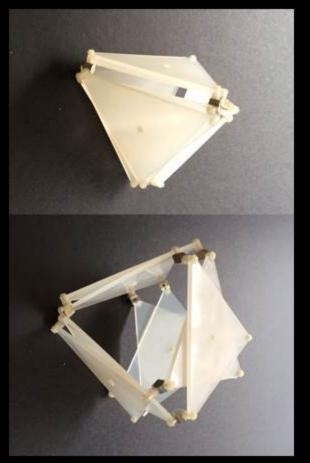
Expanding video screen, U2 world tour



Deployable materials?







Unit prototype

A prototypical collaboration



Katia Bertoldi



Applied math Mechanics of materials

Chuck Hoberman



Fine arts Mechanical engineering

Johannes Overvelde



Mechanical engineering Applied physics Applied math

James Weaver



Marine Science Molecular Biology, Chemical Engineering, Physics, Earth Sciences

objective

expressive

INVENTION

......

science

art/design

Experiments at the Wyss





3D printed (with James Weaver)



Articulated mechanics (Hoberman toy)

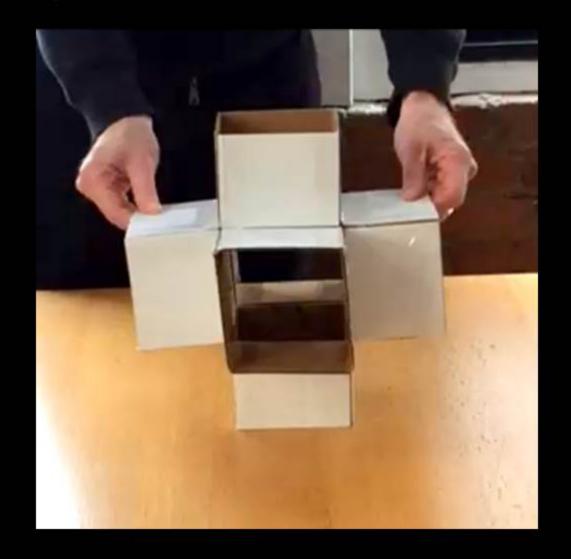


Soft material (Katia Bertoldi)

Original concept & prototype



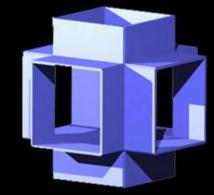
2014



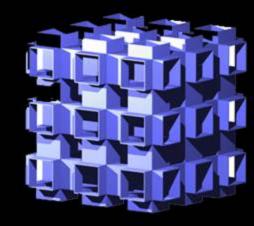
Kinetic Cuboid Structure

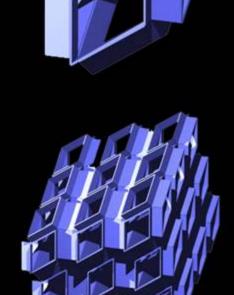
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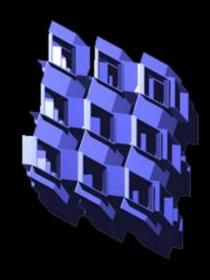






HOBERMAN

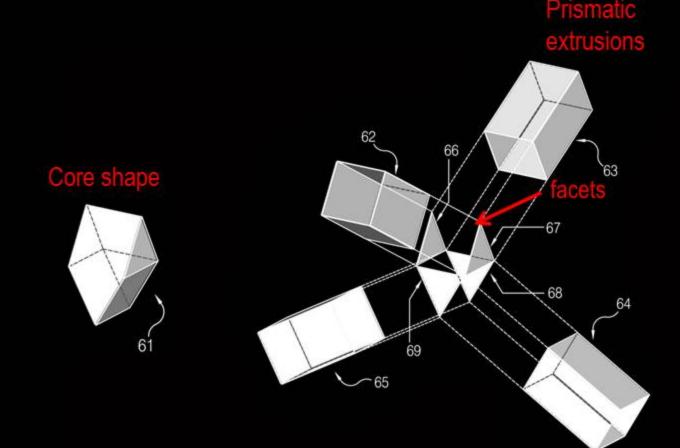


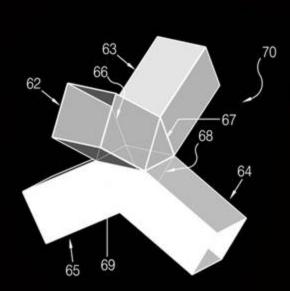




Generating a prismatic polyhedron

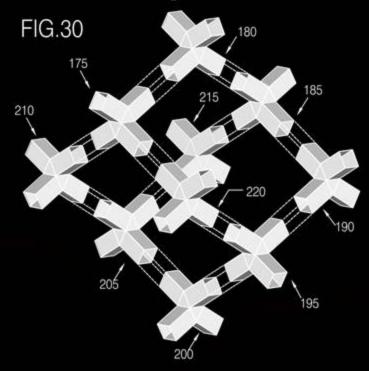


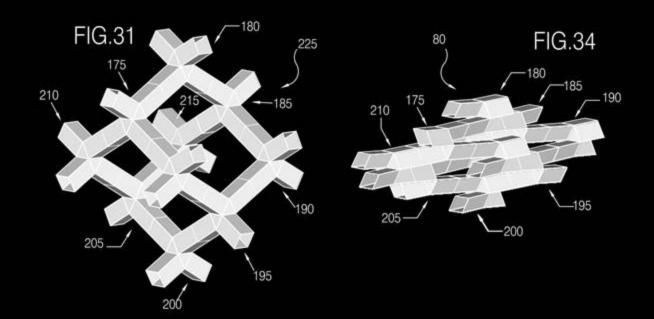




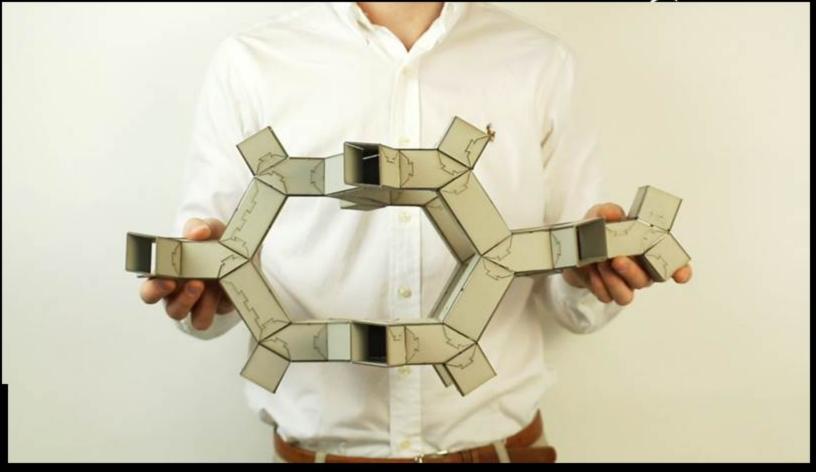


Foidable prismatic structures









Starting point: Snapology

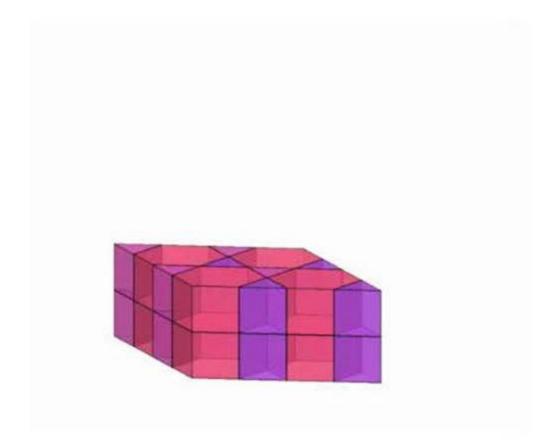
Modular origami using ribbons to create convex polyhedra



We can use these units as building block to form reconfigurable architected materials. We need a robust strategy to build them

Our design strategy

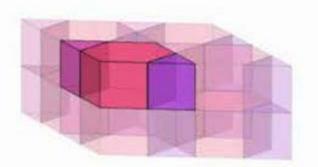




We start by selecting a space-filling assembly of convex polyhedra

Our design strategy

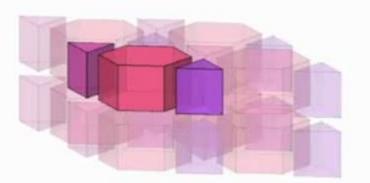




We identify the unit cell

Our design strategy





Then, we separate the polyhedra while ensuring that the normals of the face pairs remain aligned...

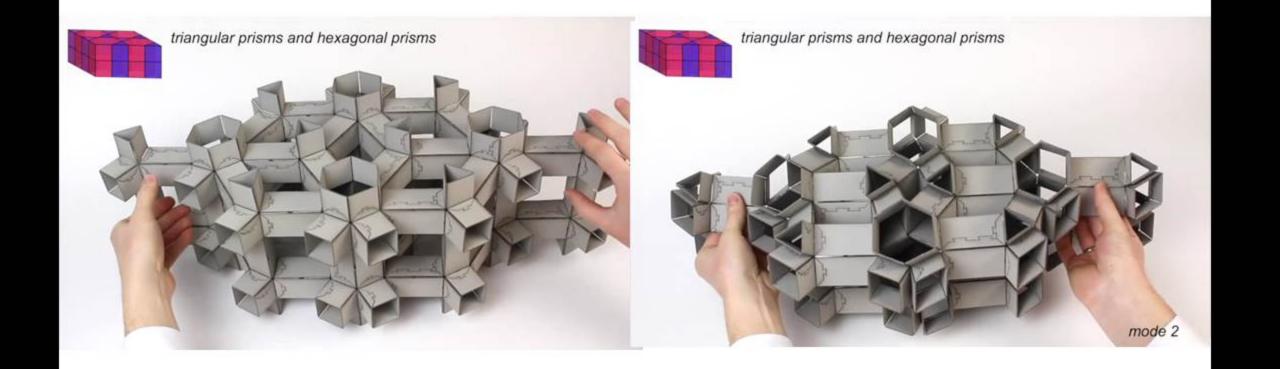
Reconfigurable prismatic architected materials



This system has 1 deformation mode

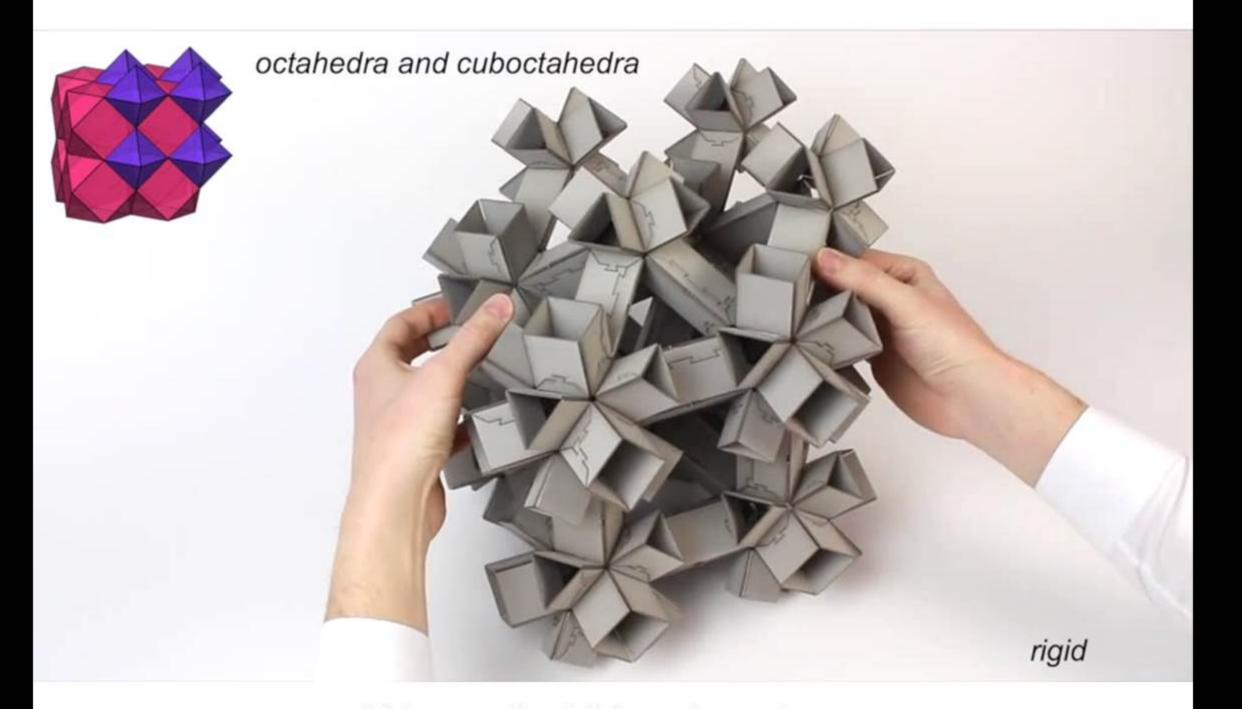
Reconfigurable prismatic architected materials





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Reconfigurable prismatic architected materials



This system has 0 deformation modes

Characterizing reconfigurability: numerical algorithm

We assume that the faces are rigid and that the hinges act as linear torsional springs

We apply periodic boundary conditions

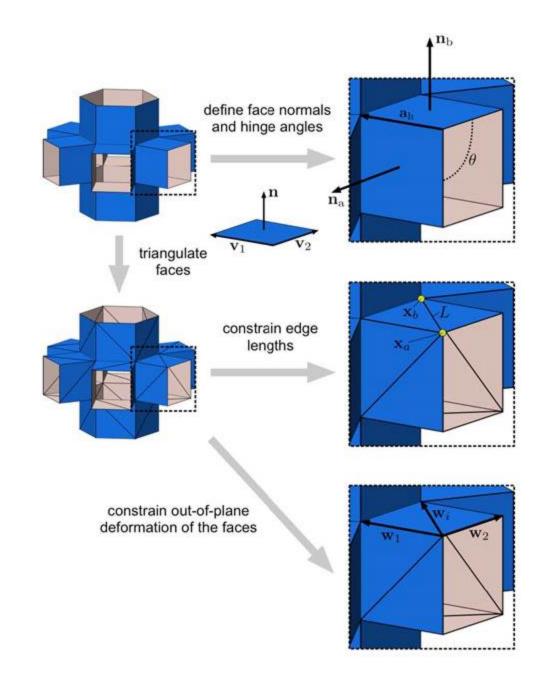
We characterize the mobility of the structure by solving

$$\tilde{\mathbf{M}}^{-1}\tilde{\mathbf{K}}\mathbf{a}_{m} = \omega^{2}\mathbf{a}_{m}$$

 ω is the an eigenfrequency

 \mathbf{a}_{m} is the amplitude of the corresponding mode

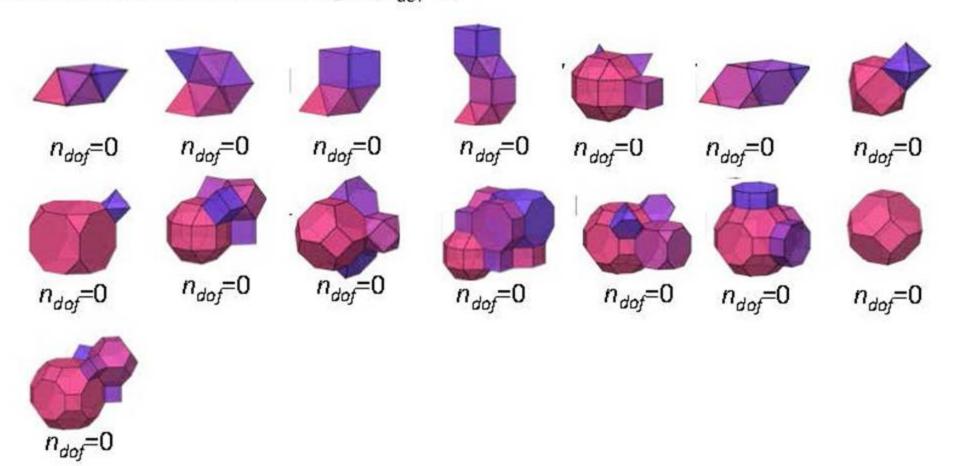
 \widetilde{M} and \widetilde{K} are the mass and stiffness matrices, which account for both the rigidity of the faces and the periodic boundary conditions through master-slave elimination.



Materials based on uniform space-filling tessellations

To explore the potential of the proposed systems, we focus on extruded materials based on the 28 uniform tessellations of the 3D space

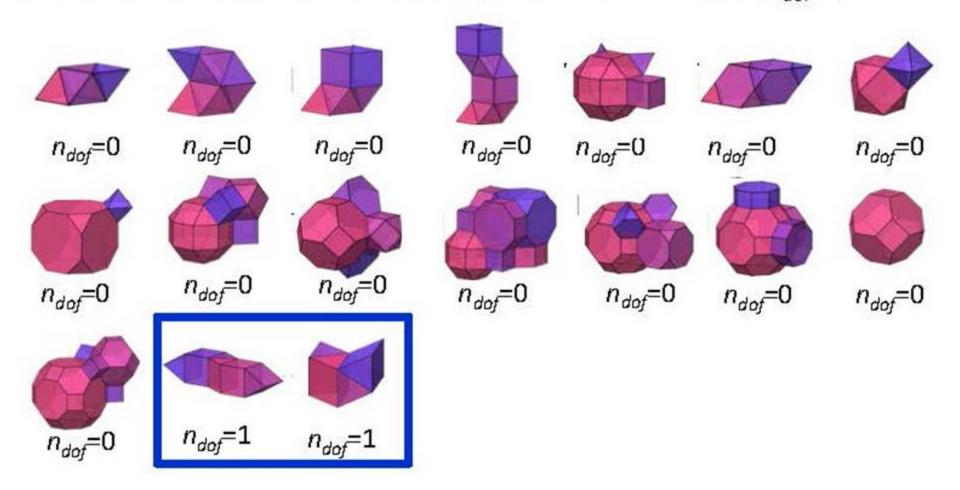
15 architected materials are rigid (n_{dof}=0)



Materials based on uniform space-filling tessellations

To explore the potential of the proposed systems, we focus on extruded materials based on the 28 uniform tessellations of the 3D space

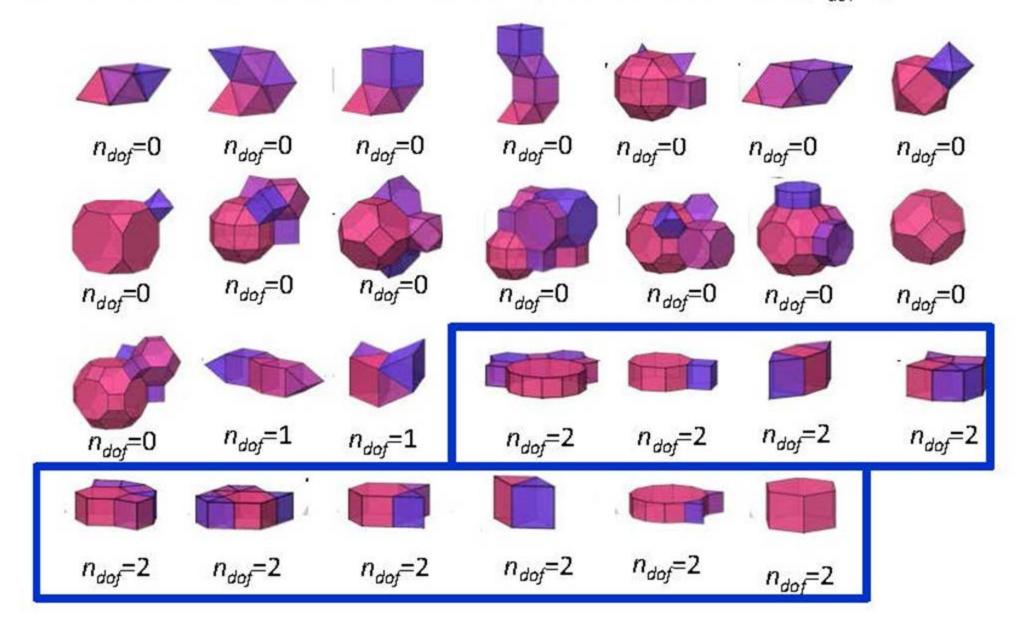
2 architected materials are characterized by 1 deformation modes (n_{dof}=1)



Materials based on uniform space-filling tessellations

To explore the potential of the proposed systems, we focus on extruded materials based on the 28 uniform tessellations of the 3D space

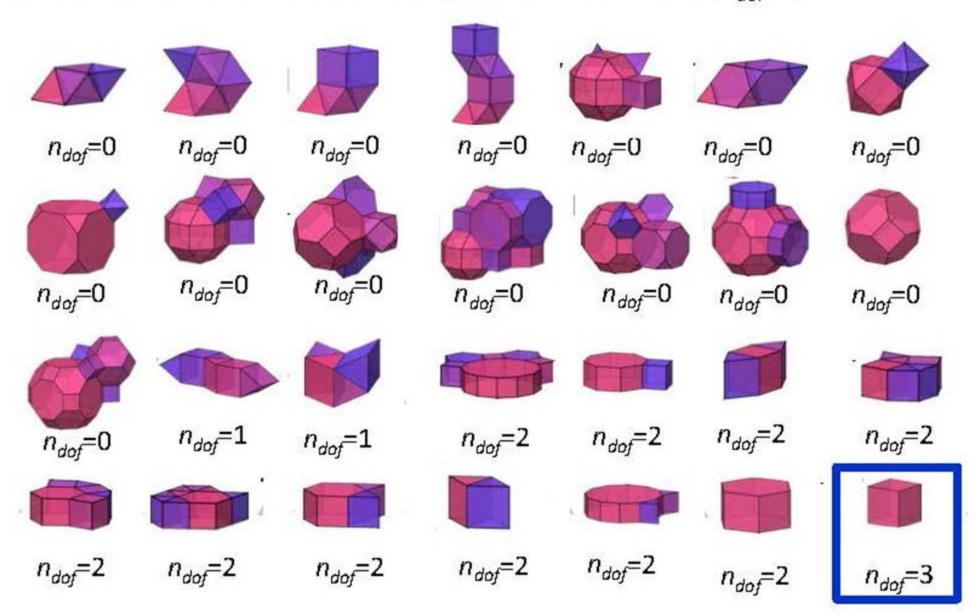
10 architected materials are characterized by 2 deformation mode (n_{dof}=2)



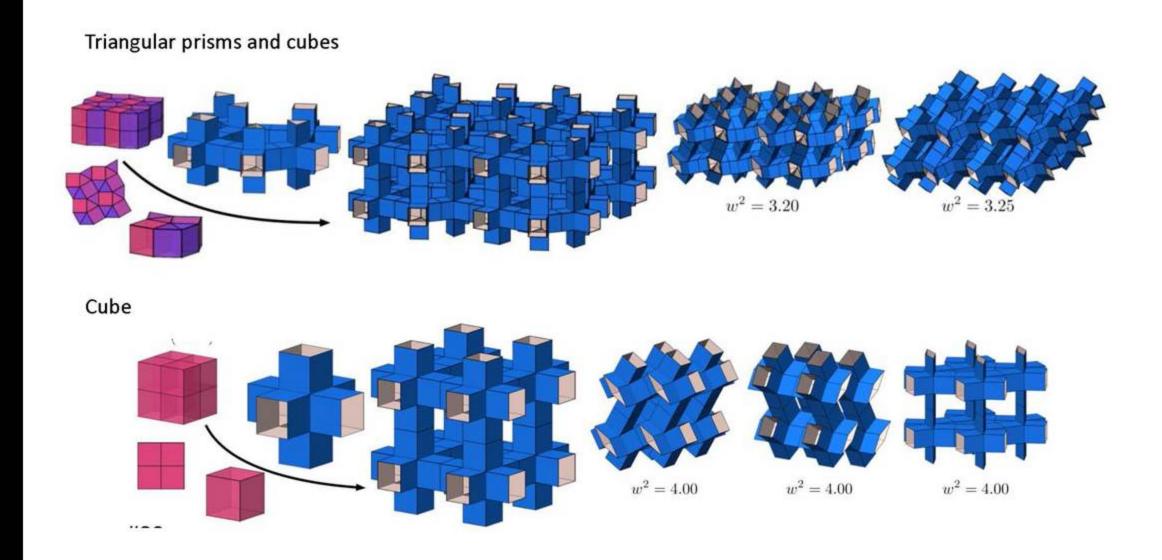
Materials based on uniform space-filling tessellations

To explore the potential of the proposed systems, we focus on extruded materials based on the 28 uniform tessellations of the 3D space

1 architected material is characterized by 3 deformation mode (n_{dof}=3)



Materials based on uniform space-filling tessellations



We characterize the macroscopic deformation associated to each mode.

Since all of them are characterized by vanishing macroscopic volumetric strain, they are all associated to shearing deformation

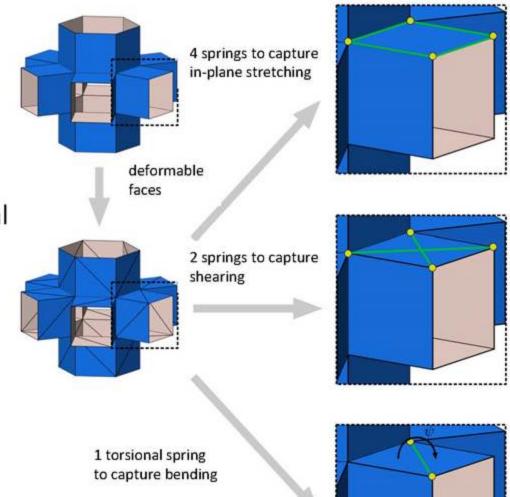
How does reconfigurability affect the mechanical properties of the system?



We now account for the faces deformability. For each rectangular face we used

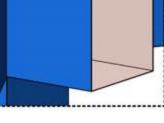
- four linear springs placed along the perimeter to capture its stretching
- two linear springs placed along the diagonal to capture its shearing
- a linear torsional spring placed along an arbitrary diagonal to capture its bending

$$E_{\text{elastic}} = E_{\text{hinge}} + E_{\text{face}}^{\text{stretch}} + E_{\text{face}}^{\text{shear}} + E_{\text{face}}^{\text{bend}},$$



Equilibrium equations:

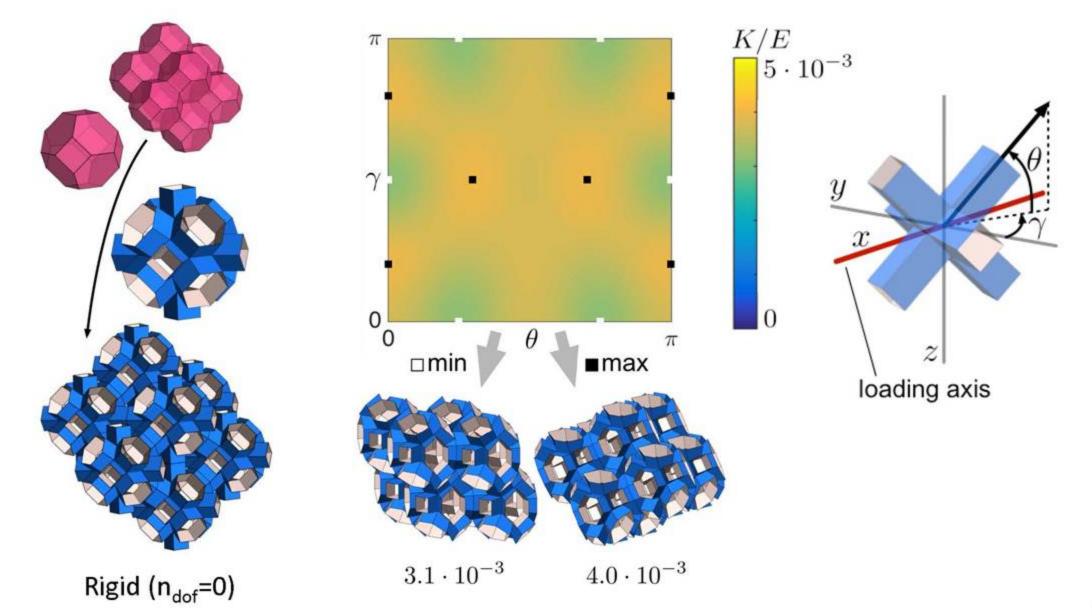
$$\frac{\partial E_{\text{potential}}}{\partial \mathbf{r}} = 0$$
 where $E_{\text{potential}} = E_{\text{elastic}} - W$



Macroscopic stiffness

Macroscopic stiffness for different loading directions

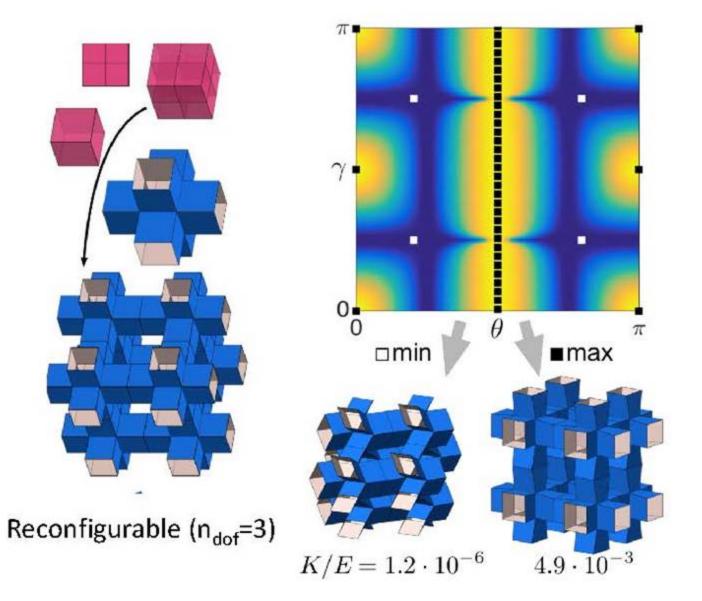
Prismatic architected material based on truncated octahedra

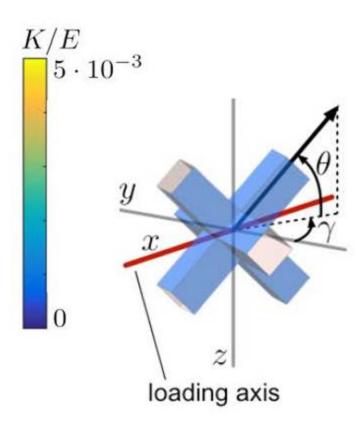


Macroscopic stiffness

Macroscopic stiffness for different loading directions

Prismatic architected material based on cube

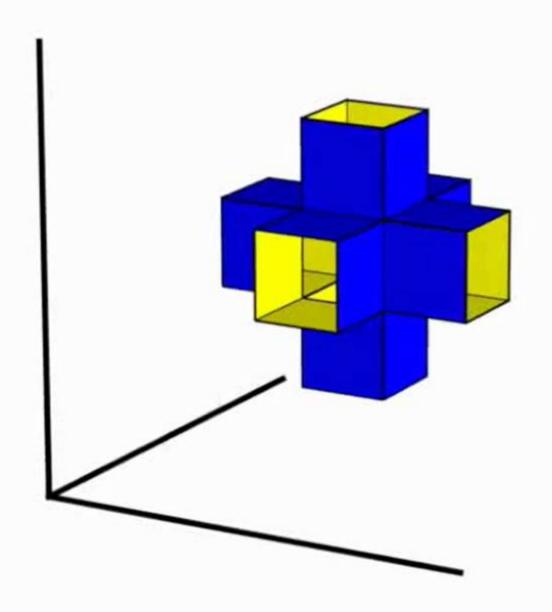


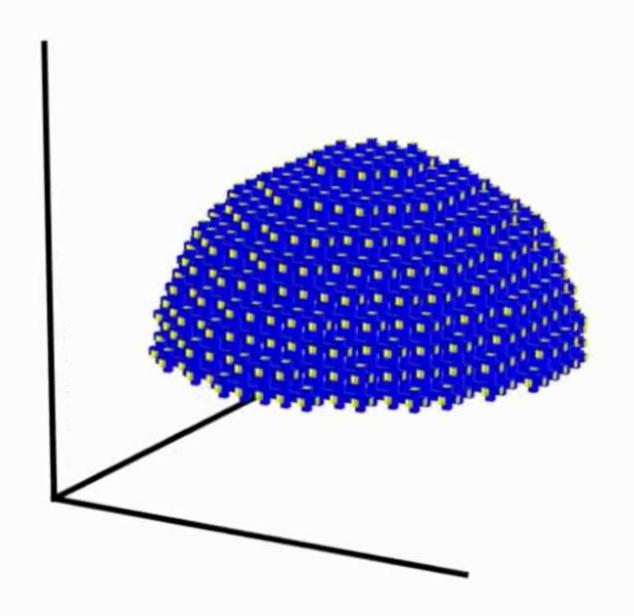


K drops in the directions for which the modes are activated

Actuated metamaterial design strategy

Dome





Applications development

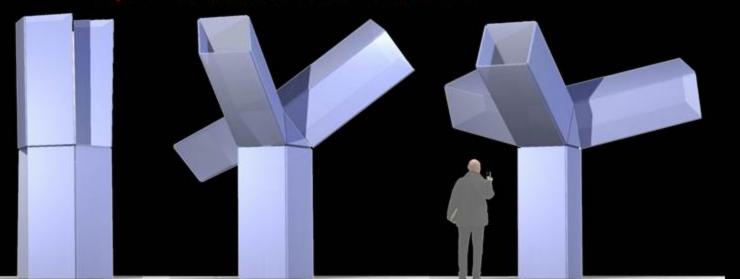






Actuated metamaterials



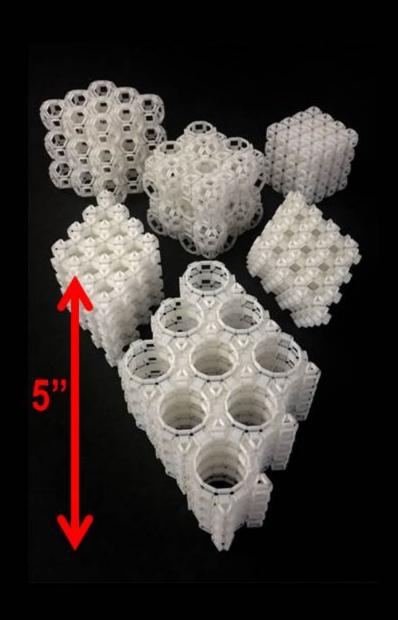


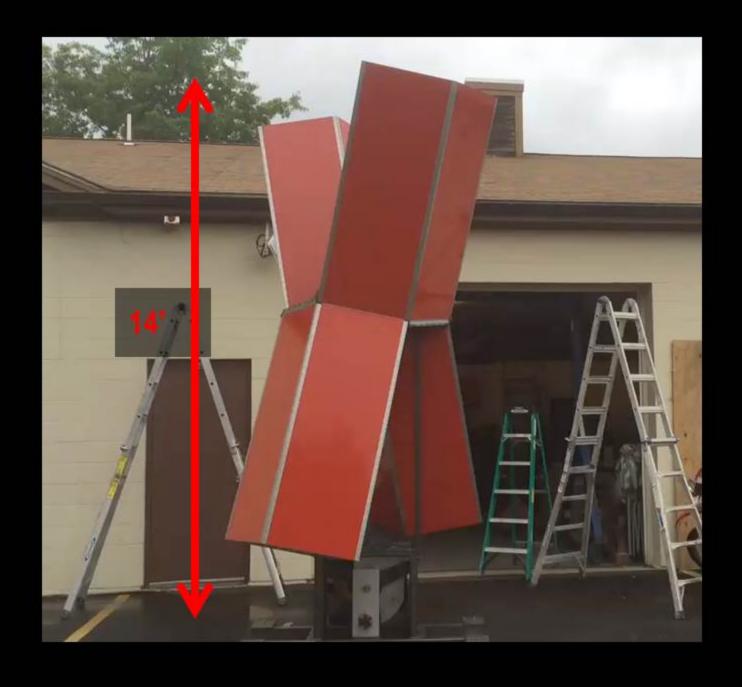
Modular robotic devices



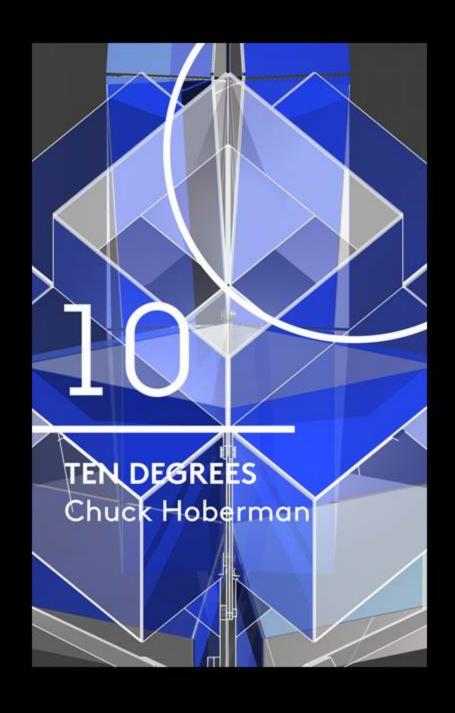
Fabrication at scale









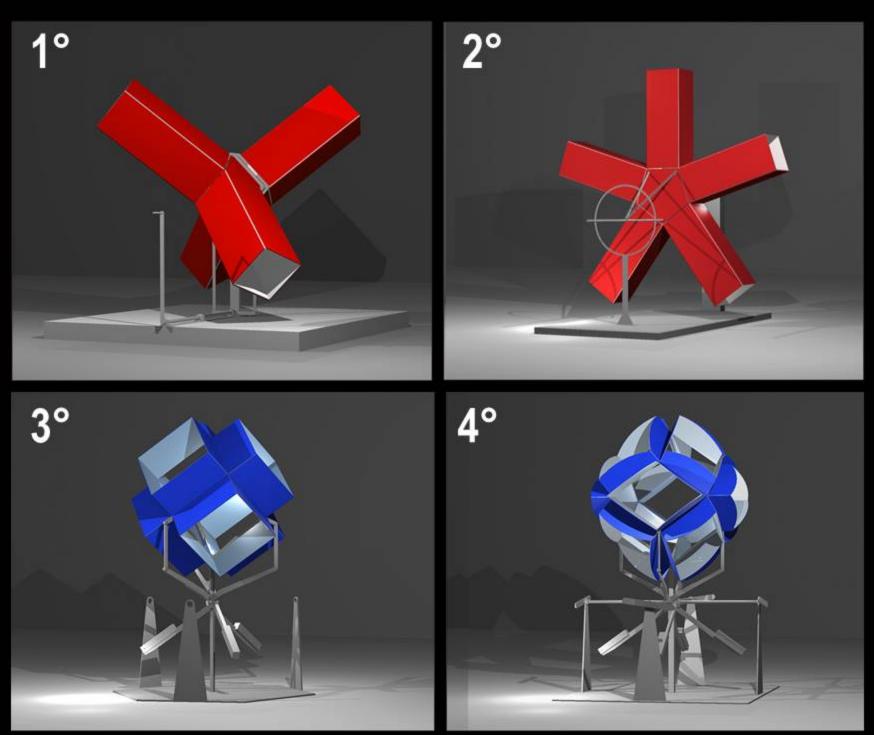


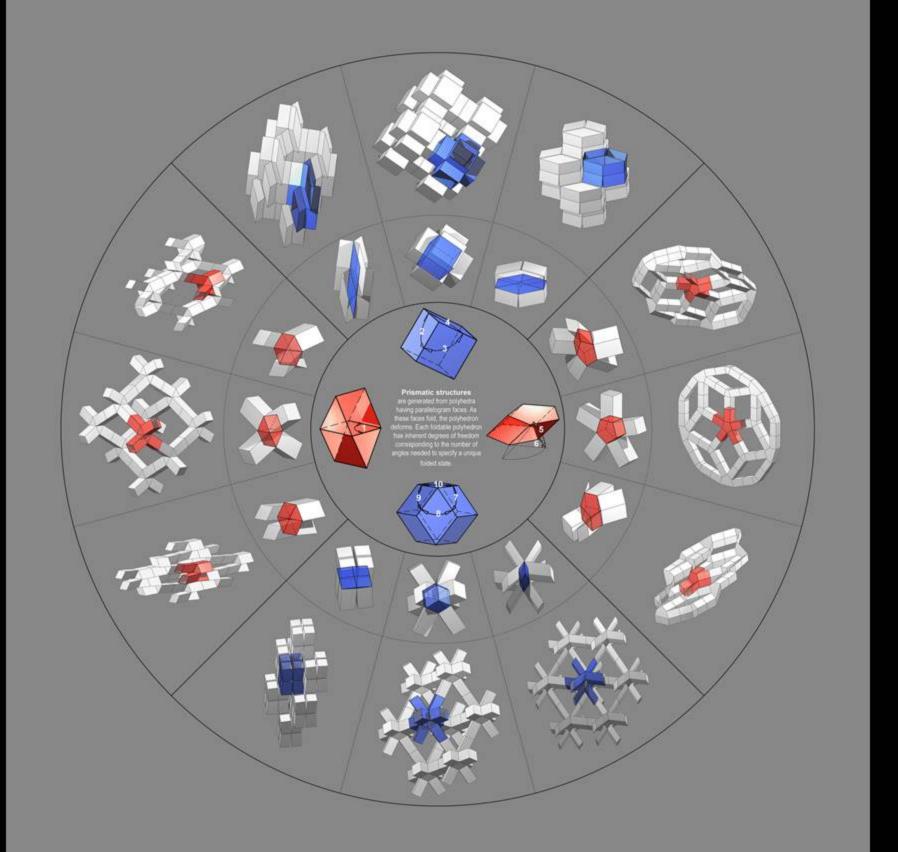


Ten degrees of freedom

Wyss S Institute

- Hands on interaction
- Collaborative control





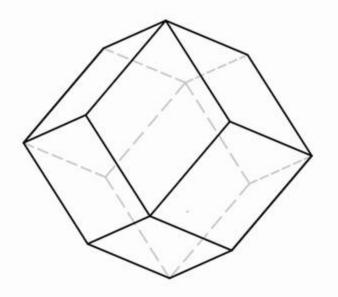


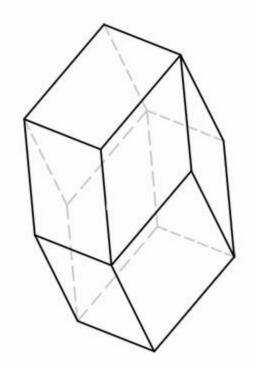






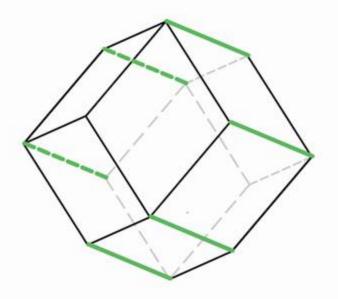


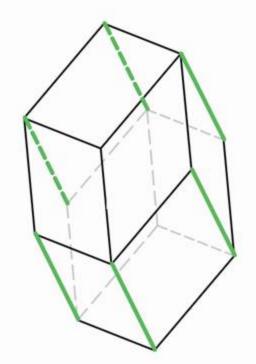




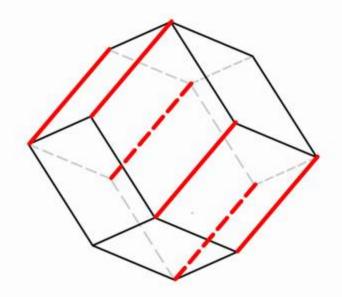
Rhombic dodecahedron – 12 faces, 24 edges

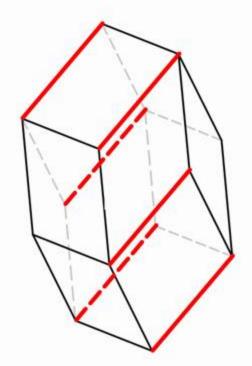




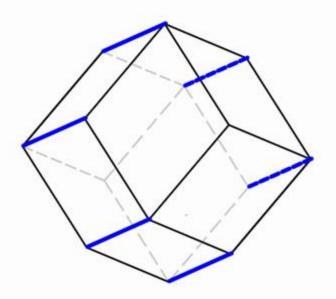


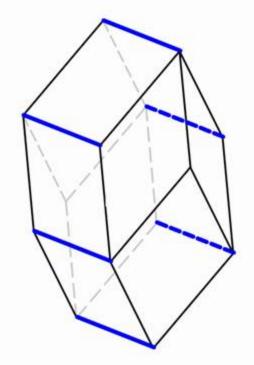




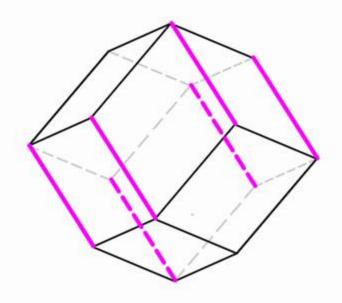


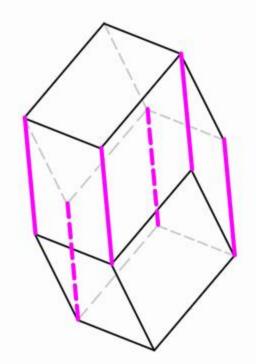




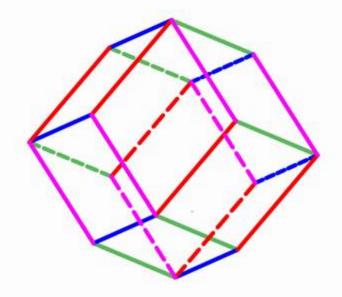


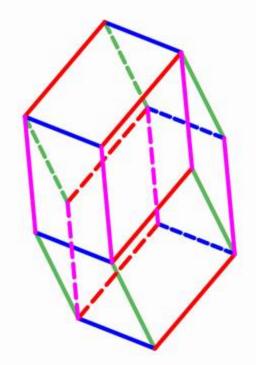






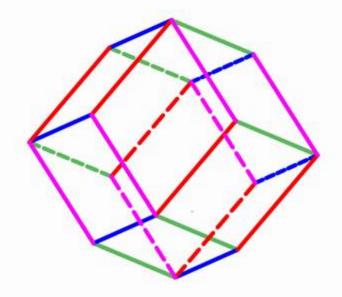


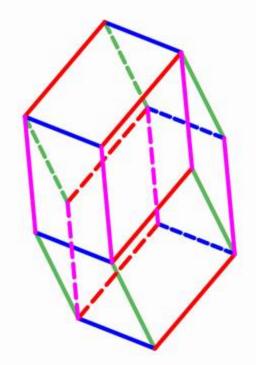




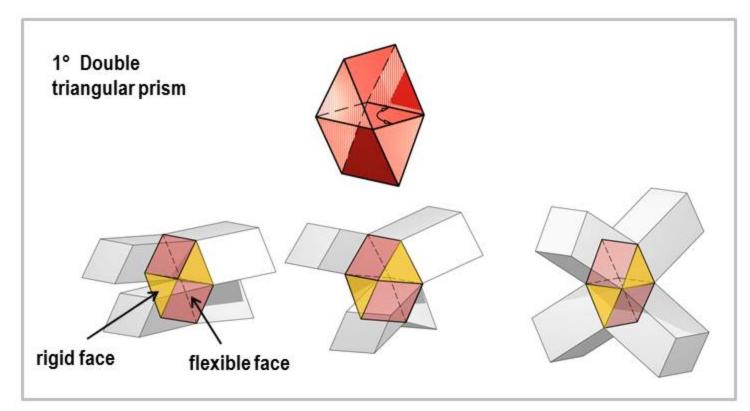
4 primary directions => 4 degrees of freedom

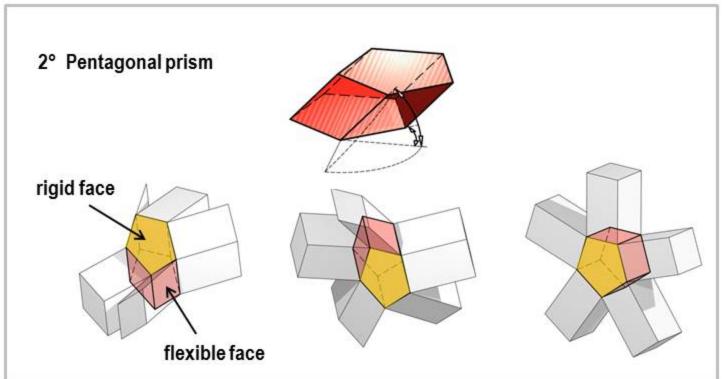


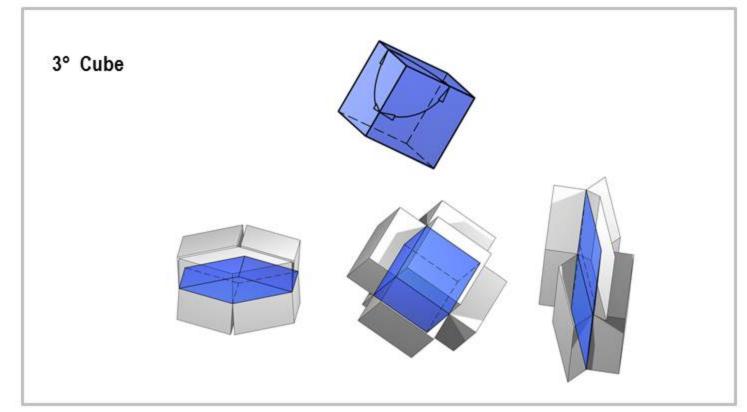


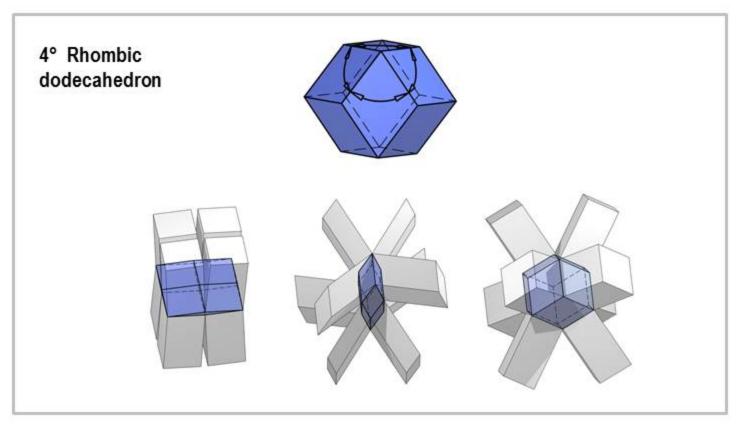


4 primary directions => 4 degrees of freedom









Thank you!



